

Structural Calculations

Van Winkle Shop Alteration
7011 78th Ave SE
Mercer Island, WA 98040

BE Project # 22028

February 18, 2022

2018 International Building Code



PROJECT VAN WINKLE PROJECT # 22028 DATE 2.17.22
 SUBJECT 7011 78TH AVE SE SHEET _____ OF _____
MERCER ISLAND BY CB

SCOPE: EXTEND ROOF OF (E) SHOP AREA TO RAISE CEILING PER ARCH.

DESIGN: ROOF 25PSF - SNOW
 WIND - 116 / 131 KZT = 1.0
 SEISMIC - 1.127 = SDS

$$\tan 18.6^\circ = \frac{x}{12}$$

$\therefore \frac{4}{12}$ SLOPE

DESIGN RAFTERS + TIES:



$$M = \frac{2' \times 13^2}{8} \times \left(\frac{25}{15}\right) = 22.78 \times \left(\frac{25}{15}\right) = 911 \text{ Ft. lb}$$

$$\frac{911 \text{ Ft. lb}}{2.5'} = 364 \text{ lb}$$

(3) 10d NAILS COLLAR TIE TO RAFTER
 @ 2/3 d

RAFTER OK - 2X2 BY INSP.

TIE OK - 2X6 BY INSP.

Wood Beam

Project File: vanwinkle.ec6

LIC# : KW-06014812, Build:20.22.3.16

BURT ENGINEERING PLLC

(c) ENERCALC INC 1983-2022

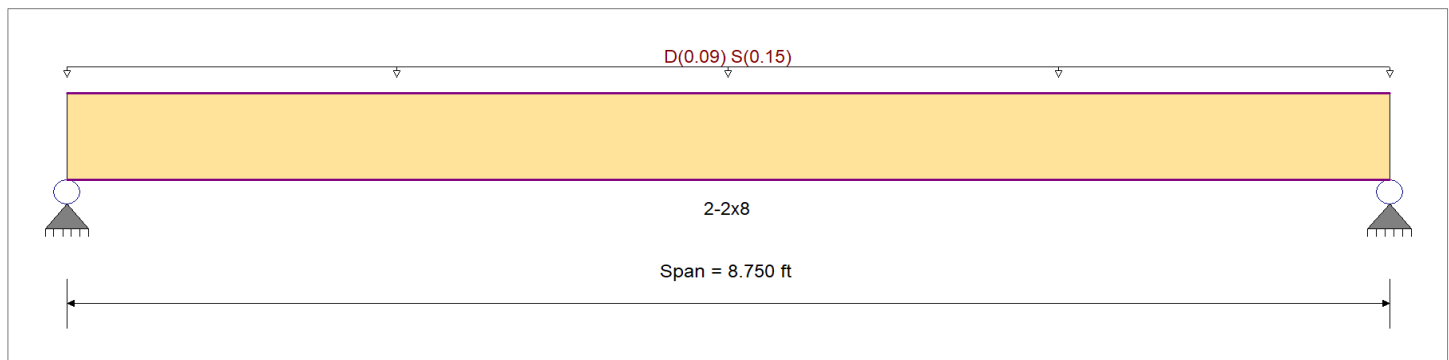
DESCRIPTION: header

CODE REFERENCES

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16
 Load Combination Set : IBC 2018

Material Properties

Analysis Method : Allowable Stress Design	Fb +	900.0 psi	E : Modulus of Elasticity	
Load Combination : IBC 2018	Fb -	900.0 psi	Ebend- xx	1,600.0ksi
	Fc - Prll	1,350.0 psi	Eminbend - xx	580.0ksi
Wood Species : Douglas Fir-Larch	Fc - Perp	625.0 psi		
Wood Grade : No.2	Fv	180.0 psi		
	Ft	575.0 psi	Density	31.210pcf
Beam Bracing : Beam is Fully Braced against lateral-torsional buckling				



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight NOT internally calculated and added
 Uniform Load : D = 0.0150, S = 0.0250 ksf, Tributary Width = 6.0 ft

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.844 : 1	Maximum Shear Stress Ratio	=	0.304 : 1
Section used for this span		2-2x8	Section used for this span		2-2x8
fb: Actual	=	1,048.75 psi	fv: Actual	=	62.90 psi
Fb: Allowable	=	1,242.00 psi	Fv: Allowable	=	207.00 psi
Load Combination		+D+S	Load Combination		+D+S
Location of maximum on span	=	4.375 ft	Location of maximum on span	=	0.000 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.131 in Ratio =	804 >=360	Span: 1 : S Only	
Max Upward Transient Deflection		0 in Ratio =	0 <360	n/a	
Max Downward Total Deflection		0.209 in Ratio =	502 >=180	Span: 1 : +D+S	
Max Upward Total Deflection		0 in Ratio =	0 <180	n/a	

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios								Moment Values			Shear Values					
			M	V	C _d	C _{F/V}	C _i	C _r	C _m	C _t	C _L	M	fb	F ^b	V	fv	F ^v		
D Only																			
Length = 8.750 ft	1	0.405	0.146	0.90	1.200	1.00	1.00	1.00	1.00	1.00	0.86	393.28	972.00	0.00	0.00	0.00	0.34	23.59	162.00
+D+S																			
Length = 8.750 ft	1	0.844	0.304	1.15	1.200	1.00	1.00	1.00	1.00	1.00	2.30	1,048.75	1242.00	0.00	0.00	0.00	0.91	62.90	207.00
+D+0.750S																			
Length = 8.750 ft	1	0.712	0.256	1.15	1.200	1.00	1.00	1.00	1.00	1.00	1.94	884.88	1242.00	0.00	0.00	0.00	0.77	53.07	207.00
+0.60D																			
Length = 8.750 ft	1	0.137	0.049	1.60	1.200	1.00	1.00	1.00	1.00	1.00	0.52	235.97	1728.00	0.00	0.00	0.00	0.21	14.15	288.00

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+S	1	0.2089	4.407		0.0000	0.000

Burt Engineering PLLC
 18530 Meridian Ave N
 Shoreline, WA 98133
 cb@burtengineering.com
 206-779-6856

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Printed: 22 MAR 2022, 1:38AM

Wood Beam

Project File: vanwinkle.ec6

LIC# : KW-06014812, Build:20.22.3.16

BURT ENGINEERING PLLC

(c) ENERCALC INC 1983-2022

DESCRIPTION: header

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0783 in	4.407 ft	0.0000 in	0.000 ft
+D+S	1	0.2089 in	4.407 ft	0.0000 in	0.000 ft
+D+0.750S	1	0.1762 in	4.407 ft	0.0000 in	0.000 ft
+0.60D	1	0.0470 in	4.407 ft	0.0000 in	0.000 ft
S Only	1	0.1305 in	4.407 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Overall MAXimum	1.050	1.050
Overall MINimum	0.656	0.656
D Only	0.394	0.394
+D+S	1.050	1.050
+D+0.750S	0.886	0.886
+0.60D	0.236	0.236
S Only	0.656	0.656

PROJECT VAN WINKLE PROJECT # 22028 DATE 2.17.22
SUBJECT 7011 78TH AVE SE SHEET _____ OF _____
MERCER ISLAND BY CB

CHECK SHEARWALLS @ OUTER END -

2'-4" WIDE

7'-10" TALL. DOWEL $\frac{2.33}{7.83} = 3.36$

$$\frac{7.83}{2.33} = 3.36$$

$$3.36 < 3.5 \text{ ok}$$

ASPECT RATIO:

$$1.25 = 0.125 \left(\frac{h}{l} \right) = 1.25 = 0.125(3.36) \\ \approx 0.83$$

SEISMIC: $V = C_s W \times P = 1.0$

$$W = 21' \times 14' \times 20 \text{ psf} = 5880$$

$$V = \frac{1.137 \times 5880}{6.5(1.4)} = 734 \text{ lb TOTAL}$$

1/2 TO OUTER WALL @ 6 BY INSP.

PROJECT VAN WINKLE PROJECT # 22028 DATE 2.17.22
SUBJECT 7011 78TH AVE SE SHEET _____ OF _____
MERCER ISLAND BY CB

$$WMD: 16 \text{ PSE} \times \frac{10' + 2'}{2} = 112 \text{ PIF}$$

$$112 \times \frac{21'}{2} = 11780$$

$$WMD \text{ CONTROLS} : \frac{11780}{2} = 5890 \text{ lb} \div 4.66' = 1264 \text{ PIF}$$

$$\frac{1264}{0.83} = 1523 \text{ lb} \leftarrow \text{wb, NO HOLDDOWN.}$$

ANCHORS INTO (K) FOUNDATION

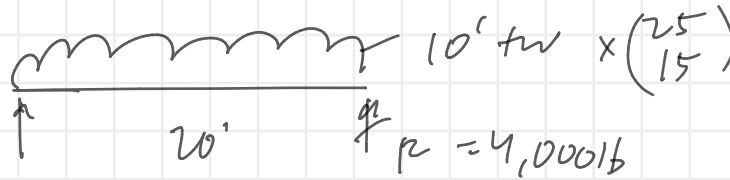
PROJECT _____ PROJECT # _____ DATE _____

SUBJECT _____ SHEET _____ OF _____

BY _____

DESIGN BEAM @ CUT-OFF

CHECK REDUCED GUB: 9'2x18 24F-V4

DEMO A PORTION
OF BEAM:

$$\text{FOOTING: } \frac{4000}{1500} = 2.67$$

→ F210 O.K. 2'-0" x 2'-0" x 10" w / (3) #4 E-w



7011 78th Ave SE, Mercer Island, WA 98040, USA

Latitude, Longitude: 47.57228449999999, -122.2342177



Date	2/17/2022, 10:58:56 PM
Design Code Reference Document	ASCE7-16
Risk Category	II
Site Class	D - Default (See Section 11.4.3)

Type	Value	Description
S_S	1.422	MCE_R ground motion. (for 0.2 second period)
S_1	0.494	MCE_R ground motion. (for 1.0s period)
S_{MS}	1.706	Site-modified spectral acceleration value
S_{M1}	null -See Section 11.4.8	Site-modified spectral acceleration value
S_{DS}	1.137	Numeric seismic design value at 0.2 second SA
S_{D1}	null -See Section 11.4.8	Numeric seismic design value at 1.0 second SA

Type	Value	Description
SDC	null -See Section 11.4.8	Seismic design category
F_a	1.2	Site amplification factor at 0.2 second
F_v	null -See Section 11.4.8	Site amplification factor at 1.0 second
PGA	0.609	MCE_G peak ground acceleration
F_{PGA}	1.2	Site amplification factor at PGA
PGA_M	0.73	Site modified peak ground acceleration
T_L	6	Long-period transition period in seconds
S_{sRT}	1.422	Probabilistic risk-targeted ground motion. (0.2 second)
S_{sUH}	1.576	Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration
S_{sD}	3.633	Factored deterministic acceleration value. (0.2 second)
S_{1RT}	0.494	Probabilistic risk-targeted ground motion. (1.0 second)
S_{1UH}	0.551	Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration.
S_{1D}	1.45	Factored deterministic acceleration value. (1.0 second)
$PGAd$	1.237	Factored deterministic acceleration value. (Peak Ground Acceleration)
C_{RS}	0.902	Mapped value of the risk coefficient at short periods
C_{R1}	0.897	Mapped value of the risk coefficient at a period of 1 s